

Summary of TM mode

$$\omega_{mnp}^{TM} = \frac{1}{\sqrt{\mu\epsilon}} \sqrt{\left(\frac{x_{mn}}{R}\right)^2 + \left(\frac{p\pi}{L}\right)^2}; \begin{cases} m = 0, 1, 2, \dots \\ n = 1, 2, 3, \dots \\ p = 0, 1, 2, \dots \end{cases} \rightarrow \begin{cases} x_{0n} = 2.405, 5.520, 8.564, \dots \\ x_{1n} = 3.832, 7.016, 10.714, \dots \\ x_{2n} = 5.136, 8.417, 11.620, \dots \end{cases}$$

$$E_r(r, \phi, z, t) = -E_0 \left(\frac{p\pi}{x_{mn}} \frac{R}{L} \right) \left[\left(\frac{m}{x_{mn}} \frac{R}{r} \right) J_m \left(x_{mn} \frac{r}{R} \right) - J_{m+1} \left(x_{mn} \frac{r}{R} \right) \right] \cos(m\phi) \sin \left(p\pi \frac{z}{L} \right) \cos(\omega_{mnp}^{TM} t)$$

$$E_\phi(r, \phi, z, t) = E_0 \left(\frac{p\pi}{x_{mn}} \frac{R}{L} \right) \left(\frac{m}{x_{mn}} \frac{R}{r} \right) J_m \left(x_{mn} \frac{r}{R} \right) \sin(m\phi) \sin \left(p\pi \frac{z}{L} \right) \cos(\omega_{mnp}^{TM} t)$$

$$E_z(r, \phi, z, t) = E_0 J_m \left(x_{mn} \frac{r}{R} \right) \cos(m\phi) \cos \left(p\pi \frac{z}{L} \right) \cos(\omega_{mnp}^{TM} t)$$

$$B_r(r, \phi, z, t) = E_0 \sqrt{\mu\epsilon} \left(\frac{R}{x_{mn}} \sqrt{\mu\epsilon} \omega_{mnp}^{TM} \right) \left(\frac{m}{x_{mn}} \frac{R}{r} \right) J_m \left(x_{mn} \frac{r}{R} \right) \sin(m\phi) \cos \left(p\pi \frac{z}{L} \right) \sin(\omega_{mnp}^{TM} t)$$

$$B_\phi(r, \phi, z, t) = E_0 \sqrt{\mu\epsilon} \left(\frac{R}{x_{mn}} \sqrt{\mu\epsilon} \omega_{mnp}^{TM} \right) \left[\left(\frac{m}{x_{mn}} \frac{R}{r} \right) J_m \left(x_{mn} \frac{r}{R} \right) - J_{m+1} \left(x_{mn} \frac{r}{R} \right) \right] \cos(m\phi) \cos \left(p\pi \frac{z}{L} \right) \sin(\omega_{mnp}^{TM} t)$$

$$B_z(r, \phi, z, t) = 0$$



Summary of TE mode

$$\omega_{mnp}^{TE} = \frac{1}{\sqrt{\mu\epsilon}} \sqrt{\left(\frac{x'_{mn}}{R}\right)^2 + \left(\frac{p\pi}{L}\right)^2}; \begin{cases} m = 0, 1, 2, \dots \\ n = 1, 2, 3, \dots \\ p = 1, 2, 3, \dots \end{cases} \rightarrow \begin{cases} x'_{0n} = 3.832, 7.016, 10.714, \dots \\ x'_{1n} = 1.841, 5.331, 8.536, \dots \\ x'_{2n} = 3.054, 6.706, 9.970, \dots \end{cases}$$

$$E_r(r, \phi, z, t) = E_0 \left(\frac{R}{x'_{mn}} \sqrt{\mu\epsilon} \omega_{mnp}^{TE} \right) \left(\frac{m}{x'_{mn}} \frac{R}{r} \right) J_m \left(x'_{mn} \frac{r}{R} \right) \sin(m\phi) \sin \left(p\pi \frac{z}{L} \right) \cos(\omega_{mnp}^{TE} t)$$

$$E_\phi(r, \phi, z, t) = E_0 \left(\frac{R}{x'_{mn}} \sqrt{\mu\epsilon} \omega_{mnp}^{TE} \right) \left[\left(\frac{m}{x'_{mn}} \frac{R}{r} \right) J_m \left(x'_{mn} \frac{r}{R} \right) - J_{m+1} \left(x'_{mn} \frac{r}{R} \right) \right] \cos(m\phi) \sin \left(p\pi \frac{z}{L} \right) \cos(\omega_{mnp}^{TE} t)$$

$$E_z(r, \phi, z, t) = 0$$

$$B_r(r, \phi, z, t) = E_0 \sqrt{\mu\epsilon} \left(\frac{p\pi}{x'_{mn}} \frac{R}{L} \right) \left[\left(\frac{m}{x'_{mn}} \frac{R}{r} \right) J_m \left(x'_{mn} \frac{r}{R} \right) - J_{m+1} \left(x'_{mn} \frac{r}{R} \right) \right] \cos(m\phi) \cos \left(p\pi \frac{z}{L} \right) \sin(\omega_{mnp}^{TE} t)$$

$$B_\phi(r, \phi, z, t) = -E_0 \sqrt{\mu\epsilon} \left(\frac{p\pi}{x'_{mn}} \frac{R}{L} \right) \left[\left(\frac{m}{x'_{mn}} \frac{R}{r} \right) J_m \left(x'_{mn} \frac{r}{R} \right) \sin(m\phi) \cos \left(p\pi \frac{z}{L} \right) \sin(\omega_{mnp}^{TE} t) \right]$$

$$B_z(r, \phi, z, t) = E_0 \sqrt{\mu\epsilon} J_m \left(x'_{mn} \frac{r}{R} \right) \cos(m\phi) \sin \left(p\pi \frac{z}{L} \right) \sin(\omega_{mnp}^{TE} t)$$



Comment on cavity geometry

- Resonant frequency

$$\omega_{mnp} = \frac{1}{\sqrt{\mu\epsilon}} \frac{1}{R} \sqrt{(x'_{mn})^2 + (p\pi)^2 (R/L)^2}$$

- not interested in large p or R : $\lim_{R \rightarrow \infty, p \rightarrow \infty} \omega_{mnp} = \frac{1}{\sqrt{\mu\epsilon}} \frac{p\pi}{L} \Rightarrow R$ -independent.
- not interested in large m or n (and/or large L): $\omega_{mnp} \rightarrow \frac{1}{\sqrt{\mu\epsilon}} \frac{x_{mn}}{R}$ for large m or n and $R/L \sim 1$ L -independent.

\Rightarrow The most interesting modes in practical applications should be low order modes with $R/L \sim 1$.



Some convenient Formulae

- Let's write the axial field for TM and TE mode as

$$\begin{aligned}\text{TM:} \quad & E_z(r, \phi) = E_0 \psi(r, \phi), \quad B_z(r, \phi) = 0; \\ \text{TE:} \quad & B_z(r, \phi) = -E_0 \sqrt{\mu\epsilon} \psi(r, \phi), \quad E_z(r, \phi) = 0;\end{aligned}$$

[note: here we introduce ψ not to be confused with the Y previously used]

- For both mode with therefore have

$$E_z^2(r, \phi) + \frac{1}{\mu\epsilon} B_z^2(r, \phi) = E_0^2 \psi^2$$



Some convenient Formulae

- From last lesson we have, for TM and TE mode

$$\begin{aligned} \begin{bmatrix} \vec{E}_t(r, \phi) \\ \vec{B}_t(r, \phi) \end{bmatrix} &= \frac{iE_0}{\gamma^2} \begin{bmatrix} \pm k \vec{\nabla}_t \\ \mu\epsilon\omega \hat{z} \times \vec{\nabla}_t \end{bmatrix} \psi(r, \phi); \\ \begin{bmatrix} \vec{E}_t(r, \phi) \\ \vec{B}_t(r, \phi) \end{bmatrix} &= \frac{i\sqrt{\mu\epsilon}E_0}{\gamma^2} \begin{bmatrix} -\omega \hat{z} \times \vec{\nabla}_t \\ \pm k \vec{\nabla}_t \end{bmatrix} \psi(r, \phi); \end{aligned}$$

- So for both mode we

$$E_t^2 + \frac{1}{\mu\epsilon} B_t^2 = \frac{E_0^2}{\gamma^4} (k^2 + \mu\epsilon\omega^2) (\nabla_t \psi)^2.$$



Computing U

- The stored energy in the resonant cavity is

$$U = \frac{1}{2} \int_V d\vec{x}^3 (ED + BH) = \frac{\epsilon}{2} \int_V d\vec{x}^3 \left(E^2 + \frac{B^2}{\mu\epsilon} \right)$$

- Note the convenient formulae

- $\int dz \sin^2(kz) = L/2$
- $\int dz \cos^2(kz) = L/2(1 + \delta_{0p})$
- Time averaging $\sin^2(\omega t)$ or $\cos^2(\omega t)$ gives 1/2



Computing U

- We also have

$$\begin{aligned}\frac{k^2 + \mu\epsilon\omega^2}{\gamma^4} &= \frac{2k^2 + (x/R)^2}{(x/R)^4} = \left(\frac{R}{x}\right)^2 \left[1 + 2\left(\frac{kR}{x}\right)^2\right] \\ &= \left(\frac{R}{x}\right)^2 [1 + 2\xi^2] \text{ where } \xi \equiv \frac{p\pi R}{xL}.\end{aligned}$$

- So integrating (by head) over z and t -averaging gives

$$U = \frac{1 + \delta_{0p}}{8} \epsilon E_0^2 L \int_A dA \left\{ \left(\frac{R}{x}\right)^2 [1 + 2\xi^2] (\nabla_t \psi)^2 + \psi^2 \right\}.$$



Computing U

- Consider $\int_A dA (\nabla_t \psi)^2$

- We have

$$\begin{aligned} \int_A dA (\nabla_t \psi)^2 &= \int_A dA \vec{\nabla}_t \cdot (\psi \vec{\nabla}_t \psi) - \int_A \psi \nabla_t^2 \psi \\ &= \oint_C dl \psi \hat{n} \cdot \vec{\nabla}_t \psi - \int_A dA \psi \nabla_t^2 \psi. \end{aligned}$$

- But the boundary conditions gives

$$\oint_C dl \psi \hat{n} \cdot \vec{\nabla}_t \psi = 0 \left\{ \begin{array}{l} \psi^{TM}(r=R) = 0 \\ \partial_r \psi^{TE}(r=R) = 0 \end{array} \right.$$

- And from wave eqn. $\nabla_t^2 \psi = -(k^2 - \mu \epsilon \omega^2) \psi = (x/R)^2 \psi$
- So finally

$$\int_A dA (\nabla_t)^2 = \left(\frac{x}{R} \right)^2 \int_A dA \psi^2,$$



Computing U

- So we end-up with JDJ Eq. 8.92

$$U = \frac{\epsilon L}{4} E_0^2 (1 + \delta_{0p}) [1 + \xi^2] \int_A dA \psi^2$$

- To perform the integral consider $\psi^2 \propto \cos^2(m\phi)$ so that $\int_0^{2\pi} d\phi \psi^2 \rightarrow \pi(1 + \delta_{0m}) J^2$ and

$$U = \frac{\pi}{4} \epsilon L E_0^2 (1 + \delta_{0m}) (1 + \delta_{0p}) [1 + \xi^2] \int_0^R dr r J_m^2 \left(x \frac{r}{R} \right).$$

- To continue we now need to specialize to either TM or TE modes...



U for TM mode

- The integral is straightforward

$$\int_0^R dr r J_m^2\left(\frac{xr}{R}\right) = \frac{1}{2} R^2 J_{m+1}^2(x_{mn})$$

the identity $\int_0^1 dx x J_\nu^2(\alpha x) = \frac{1}{2} J_{\nu+1}^2$ if $J_\nu(\alpha) = 0$ was used

- And finally the stored energy associated to the TM mode is

$$U_{mnp}^{TM} = \frac{1}{8} V \epsilon E_0^2 (1 + \delta_{0m})(1 + \delta_{0p}) [1 + \xi^2] J_{m+1}^2(x_{mn}).$$

wherein $V \equiv \pi R^2 L$



U for TE mode

- Consider the identity

$$\int_0^x d\rho \rho J_m^2(\rho) = \frac{1}{2}x^2 [J_m^2(x) + J_{m-1}^2(x)] - mxJ_m(x)J_{m-1}(x)$$

- Applied to our radial integral this gives

$$\begin{aligned} \Rightarrow \int_0^R dr r J_m^2\left(x \frac{r}{R}\right) &= \frac{R^2}{x^2} \left\{ \frac{1}{2}x^2 [\dots] - m\dots \right\} \\ &= \frac{1}{2}R^2 [J_m^2(x'_{mn}) + J_{m-1}^2(x'_{mn})] - \frac{m}{x'_{mn}}R^2 J_m(x'_{mn})J_{m-1}(x'_{mn}), \end{aligned}$$

the identity $\frac{m}{x'}J_m(x') = J_{m+1}(x') = J_{m-1}(x')$ is then used

$$\begin{aligned} \int_0^R dr r J_m^2\left(x \frac{r}{R}\right) &= \frac{1}{2}R^2 \left[1 + \left(\frac{m}{x'}\right)^2 \right] J_m^2(x') - R^2 \left(\frac{m}{x'}\right)^2 J_m^2(x') \\ &= \frac{1}{2}R^2 \left[1 - \left(\frac{m}{x'}\right)^2 \right] J_m^2(x'). \end{aligned}$$



U for TE mode

- So finally the store energy associated to TE mode is ($\delta_{0p} = 0$ ($p \neq 0$))

$$U_{mnp}^{TE} = \frac{1}{8} V \epsilon E_0^2 (1 + \delta_{0m}) \left[1 - \left(\frac{m}{x'} \right)^2 \right] [1 + \xi'^2] J_m^2(x'_{mn}).$$

$$\delta_{0p} = 0 \quad (p \neq 0) \text{ for TE-modes,}$$

where in

$$V \equiv \pi R^2 L$$
$$\xi' = \frac{p\pi R}{x'_{mn} L}$$



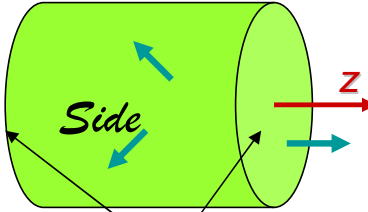
Dissipated Power

- Let's define the dissipated power per surface area

$$\frac{dP}{dA} = \frac{1}{2} R_s H_{\parallel}^2 = \frac{R_s}{2\mu^2} B_{\parallel}^2$$

Field component \parallel to cavity walls

Shunt impedance



- For a pillbox cavity

$$P = \frac{R_s}{2\mu^2} \left[\int_{side} dA B_{\parallel}^2 + 2 \int_{end} dA B_{\parallel}^2 \right].$$



P for TM mode

- For the sides of the cavity

$$\begin{aligned}\int_{side} dAB_{\parallel}^2 &= \int_0^L dz \int_0^{2\pi} d\phi R B_{\phi}^2(r, \phi, z) \\ &= \frac{L}{2} (1 + \delta_{0p}) \pi (1 + \delta_{0m}) \mu \epsilon E_0^2 [1 + \xi^2] R \left[\frac{m}{x} J_m(x) - J_{m+1}(x) \right]^2\end{aligned}$$

but $J_m(x) = 0$ so

$$\int_{side} dAB_{\parallel}^2 = \frac{1}{2} \mu \epsilon E_0^2 (\pi L R) (1 + \delta_{0p}) (1 + \delta_{0m}) [1 + \xi^2] J_{m+1}^2(x)$$

and again $\xi \equiv \frac{\pi p R}{x_{mn} L}$.



P for TM mode

- For the ends plate

$$\begin{aligned}\int_{end} dAB_{\parallel}^2 &= \int_0^{2\pi} d\phi \int_0^R dr r B_t^2 \\ &= \frac{E_0^2 \mu^2 \epsilon^2 \omega^2}{(x/R)^4} \int_A dA (\nabla \psi)^2 = \frac{E_0^2 \mu^2 \epsilon^2 \omega^2}{(x/R)^2} \int_A dA \psi^2 \\ &= \mu \epsilon E_0^2 [1 + \xi^2] \frac{\pi}{2} (1 + \delta_{0m}) R^2 J_{m+1}^2(x)\end{aligned}$$

So

$$\int_{end} dAB_{\parallel}^2 = \frac{1}{2} \mu \epsilon E_0^2 (\pi R^2) (1 + \delta_{0m}) [1 + \xi^2] J_{m+1}^2(x_{mn}).$$



P for TM mode

- In summary

$$\int_{side} dAB_{\parallel}^2 = \frac{1}{2} \mu \epsilon E_0^2 (\pi L R) (1 + \delta_{0p}) (1 + \delta_{0m}) [1 + \xi^2] J_{m+1}^2(x)$$

$$\int_{end} dAB_{\parallel}^2 = \frac{1}{2} \mu \epsilon E_0^2 (\pi R^2) (1 + \delta_{0m}) [1 + \xi^2] J_{m+1}^2(x_{mn}),$$

- So the total power loss is (with $A_s \equiv 2\pi RL$)

$$P_{mnp}^{TM} = \frac{R_s}{2\mu^2} \mu \epsilon E_0^2 \frac{1}{4} A_s (1 + \delta_{0m}) [1 + \xi^2] \left[1 + \delta_{0p} + 2\frac{R}{L} \right] J_{m+1}^2(x_{mn}).$$



P for TE mode

- Consider the side wall:

$$\begin{aligned} \int_{side} dAB_{\parallel}^2 &= \int_0^L dz \int_0^{2\pi} d\phi R [B_{\phi}^2(R, \phi, z) + B_z^2(R, \phi, z)] \\ &= \mu\epsilon E_0^2 \frac{L}{2} \pi (1 + \delta_{0m}) R \left\{ \left(\frac{m}{x'} \right)^2 J_m^2(x') \xi'^2 + J_m^2(x') \right\} \end{aligned}$$

\mathbb{P}
$$\int_{side} dAB_{\parallel}^2 = \mu\epsilon E_0^2 \frac{\pi}{2} L R (1 + \delta_{0m}) \left[1 + \left(\frac{R m p \pi}{x'^2 L} \right)^2 \right] J_m^2(x')$$

- Consider the end plates

$$\begin{aligned} \int_{end} dAB_{\parallel}^2 &= \int_0^{2\pi} d\phi \int_0^R dr r B_t^2(r, \phi, 0) \\ &= \mu\epsilon E_0^2 \xi'^2 \left(\frac{R}{x'} \right)^2 \int_A dA (\vec{\nabla} \psi)^2 \\ &= \mu\epsilon E_0^2 \xi^2 \int_A dA \psi^2. \end{aligned}$$



P for TE mode

$$\begin{aligned}\int_A dA \psi^2 &= \pi(1 + \delta_{0m}) \int_0^R dr r J_m^2\left(x' \frac{r}{R}\right) \\ &= \frac{\pi}{2} R^2 (1 + \delta_{0m}) \left[1 - \left(\frac{m}{x'}\right)^2\right] J_m^2(x')\end{aligned}$$

$$\Rightarrow \int_A dA \psi^2 = \mu \epsilon E_0^2 \frac{\pi}{2} R^2 (1 + \delta_{0m}) \xi'^2 \left[1 + \left(\frac{m}{x'_{mn}}\right)^2\right] J_m^2(x'_{mn}).$$

- So finally

$$\begin{aligned}P_{mnp}^{TE} &= \frac{R_s}{2\mu^2} \mu \epsilon E_0^2 \frac{1}{4} A_s (1 + \delta_{0m}) \left\{ 1 + \left[2\frac{R}{L} + \right. \right. \\ &\quad \left. \left. + \left(1 - 2\frac{R}{L}\right) \left(\frac{m}{x'}\right)^2 \right] \xi'^2 \right\} J_m^2(x'_{mn}).\end{aligned}$$

