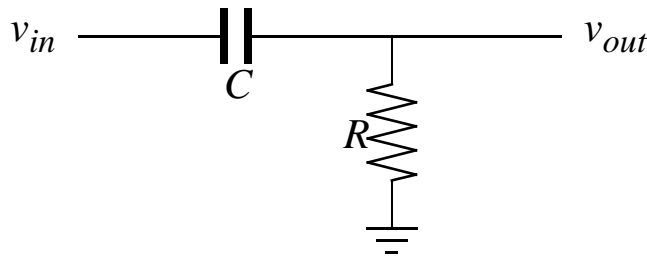


# Filter Circuits



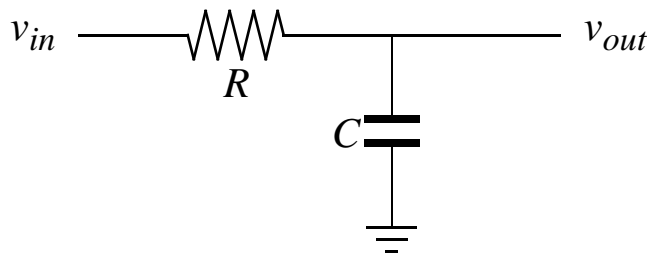
- Passive filters with a single resistor and capacitor are called one-pole filters.
- The high-pass filter selects frequencies above a breakpoint frequency  $\omega_B = 1/RC$ .



$$v_{out} = \frac{R}{R + 1/j\omega C} v_{in} = \frac{j\omega RC}{j\omega RC + 1} v_{in}$$

$$A = \left| \frac{v_{out}}{v_{in}} \right| = \frac{\omega^2 R^2 C^2}{\sqrt{1 + \omega^2 R^2 C^2}}$$

- For small  $\omega$ ,  $A$  goes as  $\omega$  or 6 dB/octave;  $\phi = \tan^{-1}(1/\omega RC)$ ; for small  $\omega$ ,  $\phi$  approaches  $+90^\circ$ .
- The low-pass filter selects frequencies below a breakpoint frequency  $\omega_B = 1/RC$ .



$$v_{out} = \frac{1/j\omega C}{R + 1/j\omega C} v_{in} = \frac{1}{j\omega RC + 1} v_{in}$$

$$A = \left| \frac{v_{out}}{v_{in}} \right| = \frac{1}{\sqrt{1 + \omega^2 R^2 C^2}}$$

- For large  $\omega$ ,  $A$  goes as  $1/\omega$  or 6 dB/octave;  $\phi = \tan^{-1}(-\omega RC)$ ; for large  $\omega$ ,  $\phi$  approaches  $-90^\circ$ .

# Transfer Function



- The complex gain for a filter is the *transfer function*.
- For a high-pass filter it is,

$$\frac{v_{out}}{v_{in}} = \frac{R}{R + 1/j\omega C} = \frac{j\omega/\omega_B}{1 + j\omega/\omega_B} \equiv H(j\omega)$$

with the breakpoint frequency  $\omega_B = 1/RC$ .

- The transfer function describes behavior as a function of frequency.
- Again for the high-pass filter, the real gain  $G(\omega) = |H(j\omega)|$

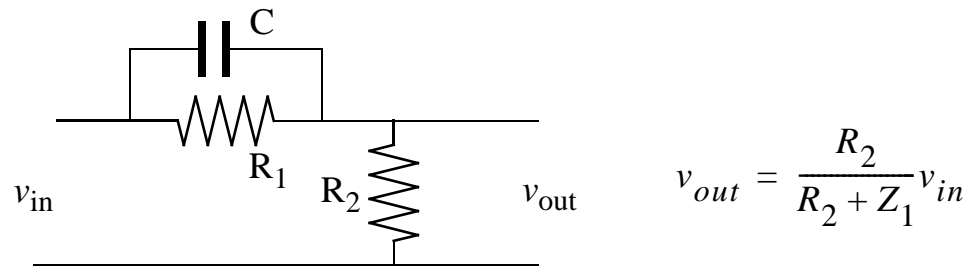
$$G(\omega) = \frac{\omega/\omega_B}{\sqrt{1 + (\omega/\omega_B)^2}}$$

falls off below  $\omega_B$  at 20 dB/decade or 6 dB/octave.

# Speed-up Capacitor



- Consider that a capacitor looks like an open connection to low  $f$  and like a short circuit at high  $f$ .



- The circuit is a resistor divider with  $R_1$  replaced with  $Z_1$  which includes a capacitor.

$$Z_1 = \frac{R/j\omega C}{R + 1/j\omega C} = \frac{R}{j\omega RC + 1}$$

- The expectation is that at high  $f$ , the divider has  $Z_1 = 0$ .

$$v_{out} = \frac{R_2}{R_2 + R_1/(j\omega R_1 C + 1)} v_{in} = \frac{j\omega R_1 R_2 C + R_2}{j\omega R_1 R_2 C + R_2 + R_1} v_{in}$$

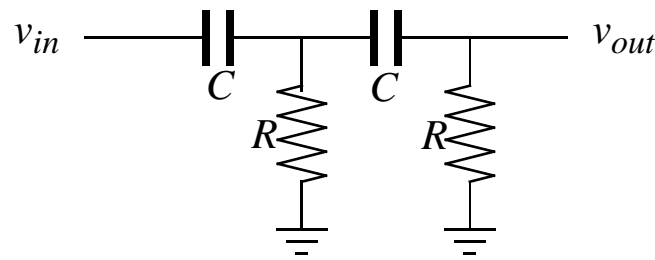
$$A = \sqrt{\frac{(\omega R_1 R_2 C)^2 + (R_2)^2}{(\omega R_1 R_2 C)^2 + (R_2 + R_1)^2}}$$

- For  $\omega \ll 1/R_1 C$ ,  $A = R_2/(R_1 + R_2)$ ;  $\omega \gg 1/R_1 C$ ,  $A = 1$ .
- High frequencies are enhanced, so a pulse edge becomes sharper

# Two-Pole Filters



- Two RC high-pass filters can be placed in series.



$$H(j\omega) = R \left( \frac{R}{2R + 1/j\omega C} \right) \left( \frac{1}{1/j\omega C + \frac{R(R + 1/j\omega C)}{2R + 1/j\omega C}} \right)$$

$$H(j\omega) = \frac{-\omega^2 R^2 C^2}{1 + 3j\omega RC - \omega^2 R^2 C^2} = \frac{-(\omega/\omega_B)^2}{1 + 3j(\omega/\omega_B) - (\omega/\omega_B)^2}$$

- The gain varies as  $\omega^2$ .

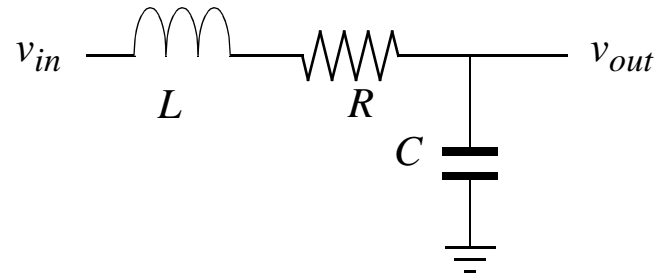
$$G(\omega) = \frac{(\omega/\omega_B)^2}{\sqrt{1 + 7(\omega/\omega_B)^2 + (\omega/\omega_B)^4}}$$

- This is a *second-order* filter.
- More poles further increase the rapidity of fall off and add phase shifts.

# RLC Filter



- A second-order low-pass filter can be made with a resistor and capacitor.



$$H(j\omega) = \frac{1/j\omega C}{j\omega L + R + 1/j\omega C} = \frac{1}{1 + j\omega/Q\omega_0 - (\omega/\omega_0)^2}$$

where  $\omega_0^2 = 1/LC$  and  $Q = \omega_0 L/R$ .

- The circuit is equivalent to a damped driven harmonic oscillator.
- There is a damping factor  $d_0 = 1/Q = R/\omega_0 L$ .

$$H(j\omega) = \frac{1}{1 + jd_0(\omega/\omega_0) - (\omega/\omega_0)^2}$$

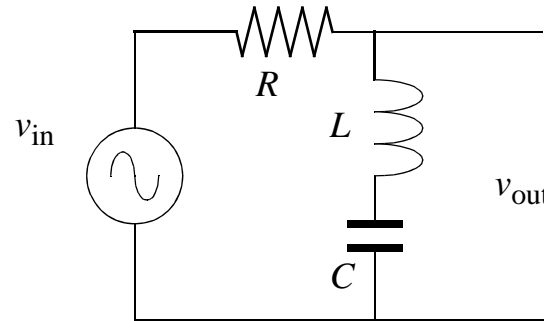
$$G(\omega) = \frac{1}{\sqrt{d_0^2(\omega/\omega_0)^2 + [1 - (\omega/\omega_0)^2]^2}}$$

- As a second-order filter, the gain varies as  $\omega^2$  above  $\omega_0$ .

# Series RLC Circuit



- An RLC circuit can form a notch filter that only negates a narrow band of frequency.



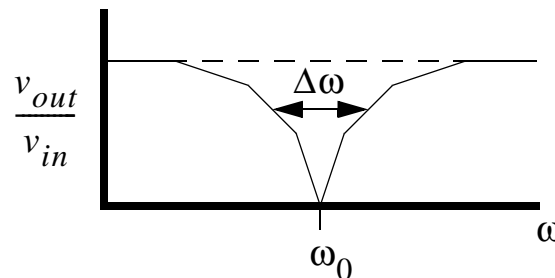
$$v_{out} = \frac{Z_{LC}}{R + Z_{LC}} v_{in}$$

$$Z_{LC} = 1/j\omega C + j\omega L = \frac{1 - \omega^2 LC}{j\omega C}$$

- The series impedance can be calculated and inserted to find the gain.  $A = \frac{v_{out}}{v_{in}} = \frac{1 - \omega^2 LC}{j\omega RC + 1 - \omega^2 LC}$

- The width of the filtered region is the Q value.  $Q = \frac{\omega_0}{\Delta\omega} = \frac{L\omega_0}{R} = R\sqrt{\frac{L}{C}}$

- A graph of the behavior shows the notch.



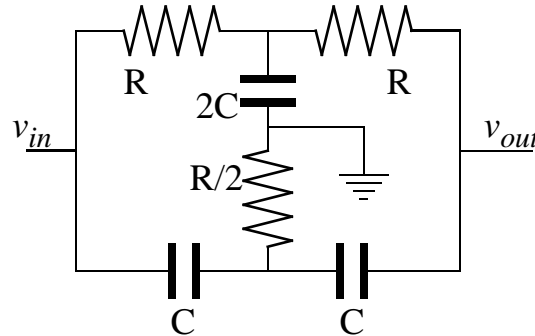
$$\Delta\omega = R/L$$

$$\omega_0 = 1/\sqrt{LC}$$

# Twin-T Filter



- A notch filter can be built with Combines two 2-pole passive filters. One is low pass, and one is high pass.



$$v_{out-LP} = \left( \frac{1/j\omega C}{R + 1/j\omega C} \right)^2 v_{in}$$

$$v_{out-HP} = \left( \frac{R}{R + 1/j\omega C} \right)^2 v_{in}$$

The combined effect of the two filters is:

$$v_{out} = \left[ \left( \frac{1}{1 + j\omega RC} \right)^2 + \left( \frac{j\omega RC}{1 + j\omega RC} \right)^2 \right] v_{in}$$

$$v_{out} = \left[ \frac{1 - (\omega RC)^2}{(1 + j\omega RC)^2} \right] v_{in}$$

At  $\omega = 1/RC$ , the gain is 0.

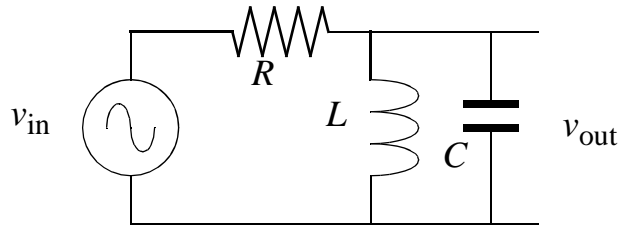
Low frequencies are shifted by  $-90^\circ$

High frequencies are shifted by  $+90^\circ$

# Parallel RLC Circuit



- If the inductor and capacitor are in parallel there is a positive resonance.



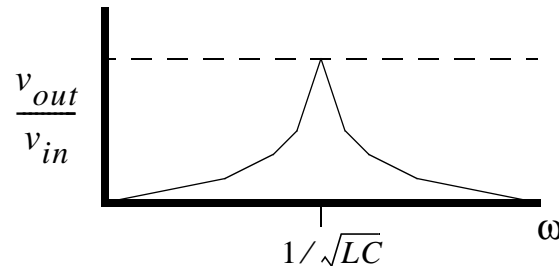
$$Z_{LC} = \frac{j\omega L / j\omega C}{1/j\omega C + j\omega L} = \frac{j\omega L}{1 - \omega^2 LC}$$

$$v_{out} = \frac{Z_{LC}}{R + Z_{LC}} v_{in}$$

- The impedance can be calculated and inserted to find the gain.

$$\frac{v_{out}}{v_{in}} = \frac{j\omega L}{R(1 - \omega^2 LC) + j\omega L} = \frac{\omega^2 L^2}{R^2(1 - \omega^2 LC)^2 + \omega^2 L^2}$$

- The filter selects only a narrow range of frequencies.

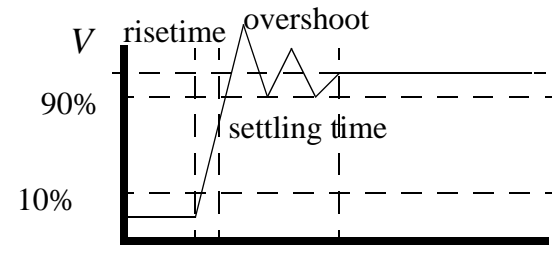




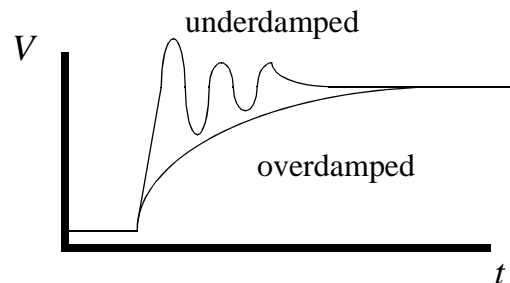
# Filter Jargon - Time Domain



- There are a number of terms used to describe the behavior of signals as a function of time.
- *Risetime*: time to get to 90% of the signal value.
- *Overshoot*: percent signal passes signal value.
- *Settling time*: time to stay within  $\epsilon$  of signal value.



- The effect of filter damping in the time domain is like a damped harmonic oscillator.



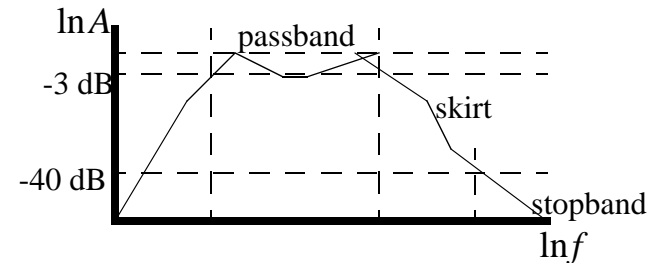
Overdamped ( $d_0 > \sqrt{2}$ ) rises slowly.

Underdamped ( $d_0 < \sqrt{2}$ ) rises quickly, but there is a ringing overshoot.

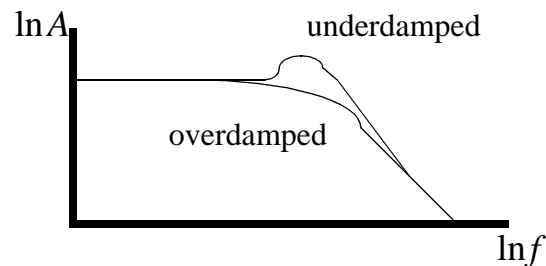
# Filter Jargon - Frequency Domain



- Filter behavior is also studied as a function of frequency.
  - *Passband*: Unattenuated region 0 to -3 dB.
  - *Cutoff frequency*: edge of passband.
  - *Ripple band*: passband that is not flat in frequency.
  - *Skirt*: transition region from -3 to -40 dB.
  - *Stopband*: frequencies with attenuation greater than -40 dB.
- Steeper skirts require more poles - higher order filter



- Damping has an effect in frequency as well as time.



High frequency ringing shows up as extra gain at resonant frequency.

Overdamped circuits have extra non-uniform gain in the passband.

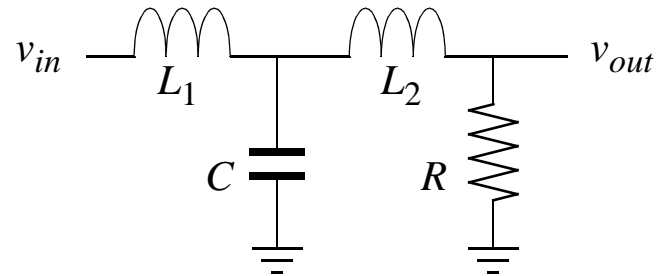
# Butterworth Filter



- Certain transfer functions give special properties to the behavior and have special names.
- A Butterworth filter is designed to give maximum flatness in the passband, so there is a critically damped response ( $d_0^2 = 2$ ) in the frequency domain.
- This creates ringing in time domain in exchange for uniform frequency response.
- The gain of a Butterworth filter is an approximation in terms of a cutoff frequency  $\omega_C$ :

$$G(j\omega)^2 = |H(j\omega)|^2 = \frac{A^2}{1 + (\omega^2/\omega_C^2)^n}$$

- A butterworth filter can be made as a passive 3-pole circuit.



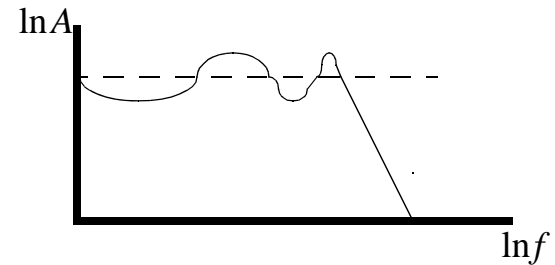
$$|H(j\omega)|^2 = \left| \left( \frac{1/j\omega C}{j\omega L_1 + 1/j\omega C} \right) \left( \frac{R}{j\omega L_2 + R} \right) \right|^2 = \frac{1}{1 + (\omega^2/\omega_C^2)^3}$$

- For  $(L_2/R)^2 = 2L_1C$ ,  $\omega_C = R^2/L_1^2L_2^2C^2$ .

# Chebyshev Filter



- A Chebyshev filter is designed to maximize the sharpness at the edge of the passband.

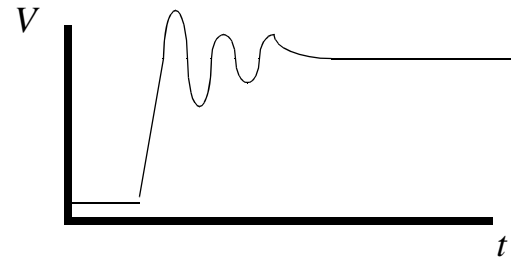


- The transfer function takes the following form.

$$|H(j\omega)|^2 = \frac{A^2}{1 + \epsilon^2 C_n^2(\omega/\omega_0)}$$

$C_n$  is an  $n$ -th order Chebyshev polynomial:  $C_n(x) = \cos[n \arccos x]$

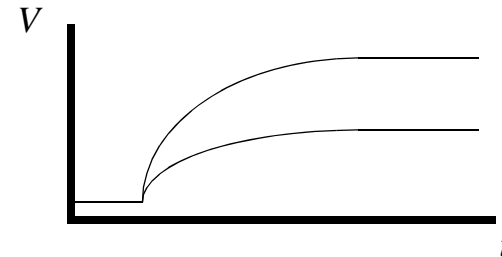
- This gives an underdamped response ( $d_0 = 0.767$ )
- There is substantial ringing in the time domain.



# Bessel Filter



- The Bessel filter gives an equal rise time independent of pulse height.



- The transfer function is as follows.

$$|H(j\omega)|^2 = \frac{A^2}{1 + \epsilon^2 B_n^2(\omega/\omega_0)}$$

where  $B_n$  is an  $n$ -th order Bessel function.

- This gives an overdamped response ( $d_0 = 1.736$ )
- There is the softer rise in the frequency domain.

